

Booster



The upper section to the right in the drawing is the 80 per cent H_2O_2 oxidizer tank. The solid fuel, probably polyurethane, is in the lower section to the left. The tail fins are detachable for ease of transportation. The nozzle will be made of pyrolytic carbon^{22,24}. Booster drawing by Anders Klyver.

Peter Madsen proposed⁵¹ a hybrid propellant

pressure fed vehicle using common nitrogen gas for pressurization of hydrogen peroxide. The concentration should be 80 per cent, which T-Stoff factory II delivers within one or 2 per cent.

The T-Stoff factory II mentioned is a hydrogen peroxide purification facility Peter Madsen built²⁷ at the end of 2013.

Hypergolic ignition would be possible

with a "consumable catalyst bed" which might be open cell polyurethane foam dusted with KMnO_4 powder. We used that at my last test in Copenhagen Suborbitals.

A catalyst bed will only be used if restart capability is required. In other words, Peter Madsen relies on thermal decomposition of H_2O_2 in the combustion chamber once catalytic ignition has occurred.

Peter later added³⁹ that a catalyst bed could be valuable in case of combustion instability. *In case of instability in the hybrid engine the combustion chamber pressure and the injector pressure may be decoupled by means of a catalyst bed.*

Engine test burns were performed⁴¹ on August 23, 2014.

Ignition failed at some occasions. Apparently the reliability of the consumable catalyst bed left something to be desired.

Peter Madsen in the following days experimented⁴² with improvements to the consumable catalyst bed but did not find

lasting improvement before the test engine suddenly exploded during a hard start⁴³.

This debug work with the consumable catalyst bed made Peter Madsen consider using a traditional catalyst bed ahead of the combustion chamber⁴⁴.

In august 2014 Peter Madsen began to consider^{45,47} steel for the oxidizer tank. He mentioned S355, S500, and S700.

Passive blow down pressurization will be used in the first *boiler plate version* of the booster. That means the oxidizer tank will contain up to 65 per cent liquid oxidizer and 35 per cent nitrogen pressurization gas²¹.

This kind of pressurization system is the most simple system known. It is the easiest system to develop and implement.

The downside is that you cannot get a high mass ratio with this system.

However, the mass ratio is not critical in the first phase of the project where altitudes like 20 km to 40 km will be considered a fine result²¹.

The nozzle will be made of pyrolytic carbon²¹ like the HEAT-1X nozzle^{22,24}. A piece with a mass of 96 kg was used. It was turned to the desired shape with the big Tyrannosaurus Rex turning lathe²⁸.

The pyrolytic carbon erosion rate is²⁶ $0.6 \frac{\text{mm}}{\text{s}}$.

Peter Madsen and his associates cast a 500 kg block of polymer²⁶ in 2011.



Ready⁴⁶ for rocket engine testing at August 23, 2014. The Horizontal Assembly Building HAB is the red building in the top of the photograph. Zone A is the rocket engine test area. Zone B is the command area. Zone C is for photographic equipment. Zone D is for the audience.

21. Peter Madsen: "Fare: teknikbasker... Hybridmotoren, set indefra". In English, "Danger: Techie knockout... The inside of the hybrid propellant engine". Published on ing.dk 2014-07-14 13:50.

22. Peter Madsen: "Hybridraketten / spåntagningsproblemet". In English, "The hybrid propellant engine / the turning chip problem". Published on ing.dk 2011-04-24 09:27.

24. Peter Madsen: "Opsendelse fra Nordsøen af HEAT måske allerede til sommer". In English, "Launch of HEAT from the North Sea possibly already this coming summer". Published on ing.dk 2009-09-23 15:02.

27. Peter Madsen: "God jul fra Peter Madsen!" In English, "Merry Christmas from Peter Madsen!" Published on ing.dk 2013-12-24 15:08.

28. Peter Madsen: "Tyrannosaurus Rex brøler!" In English, "Tyrannosaurus Rex roars!" Published on ing.dk 2011-09-15

00:53.

39. Peter Madsen: "24. juli 2014 — døgnrapport fra et Rumlaboratorium". In English, "July 24, 2014 — daily report from a Space laboratory". Published on ing.dk 2014-07-24 21:28.

41. Peter Madsen: "Lørdagens tests og chockdiamanter fra RML!" In English, "The tests of saturday and shock diamonds from RML!" Published on ing.dk 2014-08-24 15:20.

42. Peter Madsen: "Femte test af SuperHATV motoren — nu med forbedret tændsats". In English, "Fifth test of the SuperHATV motor — now with improved igniter". Published on ing.dk 2014-08-25 13:29.

43. Peter Madsen: "XLR3B-2". Published on ing.dk 2014-08-28 11:54.

44. Peter Madsen: "Jernbeton. Masser af jernbeton". In English, "Reinforced concrete. Lots of reinforced concrete". Published on ing.dk 2014-08-30 15:25.

45. Peter Madsen: "Kan man have T-stoff i en ståltank?" In English, "Will it work with T-stoff in a steel vessel?" Published on ing.dk 2014-08-17 18:36.

46. Peter Madsen: "Oprustning på Refshaleøen". In English, "Armament on Refshaleøen". Published on ing.dk 2014-08-06 23:56.

47. Peter Madsen: "Der regnes, tegnes og bygges på livet løs!" In English, "Calculation, drawing, and fabrication at full power!" Published on ing.dk 2014-08-02 01:47.

51. Peter Madsen: "Her er rumplanen!" In English, "Here is the spaceflight plan!" Published on ing.dk 2014-06-17 13:11.

Decomposition

Usually rocket engines decompose H_2O_2 by catalysis before it is injected into the engine. In this way H_2O and O_2 is injected instead of H_2O_2 .

It is known that H_2O_2 will decompose when heated. It has therefore been considered to use thermal decomposition of H_2O_2 instead of catalytic decomposition.

This can be done in a decomposition chamber before the combustion chamber, or it can be done in the combustion chamber.

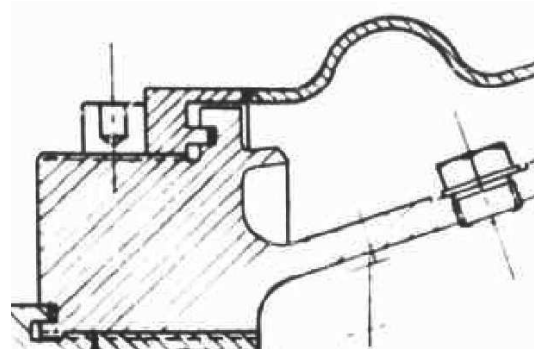
Let us first consider doing thermal decomposition in a decomposition chamber before the combustion chamber.

According to the classic Rocketdyne *Hydrogen Peroxide Handbook*⁸²⁶ thermal decomposition cannot be used in a self-sustaining way¹.

The use of self-heating thermal chambers to maintain controlled decomposition of hydrogen peroxide has been limited to laboratory studies.

Experiments concluded that¹

the slow rate of thermal decomposition of hydrogen peroxide cannot compete with the rates obtainable with catalytic decomposition.



Detail from a regeneratively cooled combustion chamber³.

Schumb et al says that although in principle²

decomposition could be obtained by a purely thermal method (...) the problems of reliable start-up and operation have always led in practice to the use of catalyst, except where direct reaction with a self-igniting [hypergolic] fuel has been used.

1. See the classic Rocketdyne *Hydrogen Peroxide Handbook*⁸²⁶ page 433, pdf page 452.

2. See Schumb et al²⁶⁸² page 109, pdf page 119.

3. The drawing is from one of the documents²⁹⁵⁵ about German rocket technology in 1935 to 1945, pdf page 102.

826. Cain, E F C et al: "Hydrogen peroxide handbook". Published by Rocketdyne and U S Air Force as AFRPL-TR-67-144, USA, July 1967.

2955. Anon: "Analysis and evaluation of German attainments and research in the liquid [propellant] rocket engine field. Volume IV. Propellant injectors". Published by Central Air Documents Office (Army - Navy - Air Force), USA, February 1952.

2682. Schumb, W C, et al: "Hydrogen peroxide. Part four. Report no. 45". Published by Massachusetts Institute of Technology as NR-092-008, USA, November 1953.

Decomposition

The United States Missile Defense Agency in 2003 proposed a project¹ to figure out how thermal decomposition of H_2O_2 could be used.

It seems the agency was open to both kinds of thermal decomposition, that is, both in a chamber for itself, and in a combustion chamber.

The agency said in the proposal that hydrogen peroxide is normally

passed over a catalyst bed to decompose it prior to entering the main combustion chamber

but the agency

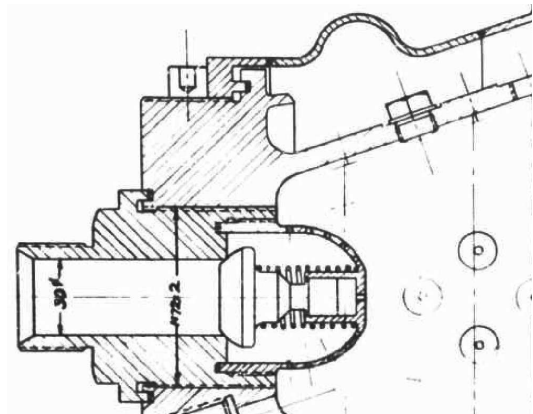
seeks alternative techniques for decomposing HTP²

The agency said that

the only other documented decomposition mechanism is thermal

but

past attempts at employing thermal decomposers frequently resulted in catastrophic failure



Detail from a regeneratively cooled combustion chamber³.

1. See the Small Business Technology Transfer Program²⁶⁹² page 8.

2. HTP is short for *high test peroxide* which means a mixture of H_2O_2 and H_2O where the concentration of H_2O_2 is close to 100 per cent.

3. The drawing is from one of the documents²⁹⁵⁵ about German rocket technology in 1935 to 1945, pdf page 102.

2955. Anon: "Analysis and evaluation of German attainments and research in the liquid [propellant] rocket engine field. Volume IV. Propellant injectors". Published by Central Air Documents Office (Army - Navy - Air Force), USA, February 1952.

2692. Anon: "Missile Defense Agency (MDA) small business technology transfer program (STTR)". Published by the Missile

Defense Agency, USA, presumably in
2003.

The vehicle

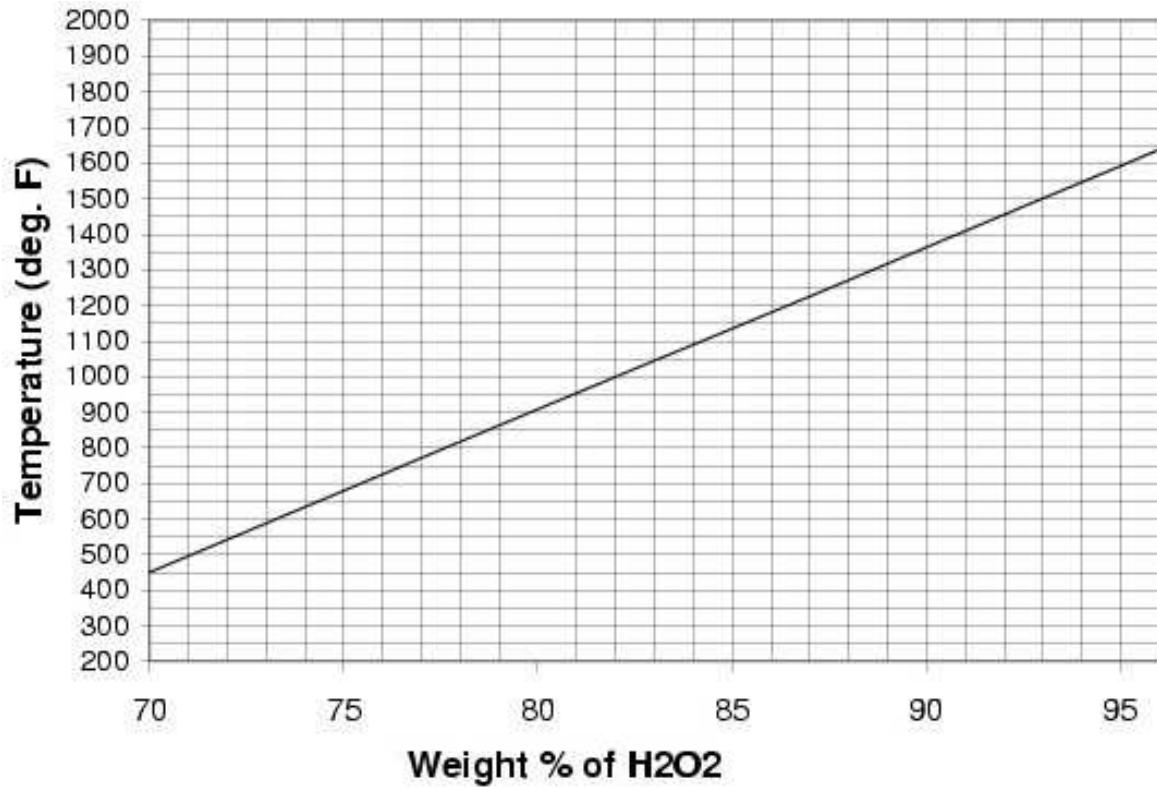
Launch mass ⁹	2.0e3 kg
Vehicle diameter ⁴⁰	0.64 m
Motor type ⁵¹	Hybrid
Grain geometry ^{6,3}	Wagon wheel
Grain ports ^{6,3}	9
Throat diameter ⁶ d_t	200 mm
Combustion chamber pressure ⁶ P_c	16 bar or 1.6 MPa at lift-off
Thrust coefficient ⁶ C_f	1.3
Throat area ^{6,7} A_t	314 cm ² or 31.4e-3 m ²
Pressurization system ⁵¹	Pressure-fed
Ignition system ¹	Consumable catalyst bed
Ignition system ²	Pellet KMnO ₄ catalyst bed
Oxidizer tank wall thickness ⁴⁷	3.0 mm if steel

Table continued at the next page.

Fuel ^{5,2943}	Solid polyurethane "Edulan Purteknik 1133 sort"
Fuel tensile strength ²⁹⁴²	7.9 MPa according to ISO 527
Fuel density ²⁹⁴²	1 110 $\frac{\text{kg}}{\text{m}^3}$ according to ISO 2781
Fuel ⁶	168 kg
Oxidizer ⁵¹	80 per cent H ₂ O ₂
Oxidizer ⁶	840 kg
Expected ISP ^{6,40}	180 s to 190 s
Expected exhaust velocity ⁸	1.76 $\frac{\text{km}}{\text{s}}$ to 1.86 $\frac{\text{km}}{\text{s}}$
Oxidizer flow at lift-off ⁶	29 $\frac{\text{kg}}{\text{s}}$
Propellant flow at lift-off ⁶ $\frac{dm}{dt}$	34.8 $\frac{\text{kg}}{\text{s}}$
Thrust at lift-off ^{6,7,8} F	62 kN

Notes on the following pages.

1. Ignition. The theoretical decomposition temperature of 80 per cent H_2O_2 is¹⁰ about 750 K or 480 C. In an engine it will take some time for the catalyst bed to heat up. At ignition time the temperature will therefore be lower than 750 K.



Decomposition temperature of H_2O_2 as a function of concentration¹⁰.

450 F is 505 K or 232 C.

900 F is 755 K or 482 C.

1. Continued from the previous page. The consumable catalyst bed was the ignition device to be used in the beginning of the project. After the problems on August 27, 2014, it seems less likely this type of ignition device will be used.

2. It is not quite right to call a catalyst bed an ignition system, so here is an explanation.

The idea is that ignition will occur automatically if the 80 per cent H_2O_2 is decomposed in a KMnO_4 catalytic pellet bed before it is injected into the combustion chamber with solid polyurethane.

The temperature of the mixture of H_2O gas and O_2 gas is about 750 K or 480 C. The melting point of polyurethane vary considerably with the kind of polyurethane. One kind of polyurethane melts at 564 K or 291 C. See the polymer data handbook¹⁷² page 879, pdf page 969. The warm H_2O and O_2 gas is therefore about 200 K above the melting point of the polymer. Therefore the polymer will melt in the surface layer.

This kind of polymer begins to decompose when it melts. It does not become liquid. So it gives off various gases, presumably mostly made of carbon and hydrogen. The question is now if some of those substances can be ignited.

The autoignition temperature of some of the organic substances given off by the decomposing polyurethane is less than 750 K, for instance 638 K or 365 C for ethanol⁴.

3. The center of mass stability of the vehicle in relation to the grain geometry has not yet been addressed.

4. Wikipedia: Ethanol.

5. Peter Madsen: Email 2014-09-03.

6. Peter Madsen: Email 2014-08-26.

7. The rocket engine thrust is

$$F = C_f * A_t * (P_c - P_a)$$

where C_f is the thrust coefficient, A_t is the throat area, P_c is the combustion chamber pressure and P_a is the ambient pressure.

With $C_f = 1.3$, $A_t = 314 \text{ cm}^2$, $P_c = 16 \text{ bar}$, and $P_a = 1.0 \text{ bar}$ we get $F = 61 \text{ kN}$.

With $C_f = 1.3$, $A_t = 31.4 \text{e-}3 \text{ m}^2$, $P_c = 1.6 \text{ MPa}$, and $P_a = 0.10 \text{ MPa}$ we get $F = 61 \text{ kN}$. 8. The exhaust velocity is $V_e = g * \text{ISP}$ where g is the acceleration of Earth. The engine thrust is

$$F = V_e * \frac{dm}{dt}$$

With $V_e = 1.76 \frac{\text{km}}{\text{s}}$ and $\frac{dm}{dt} = 34.8 \frac{\text{kg}}{\text{s}}$ we get $F = 61 \text{ kN}$.

9. The launch mass is calculated from the an assumption of a geometrical lift-off acceleration of $20 \frac{\text{m}}{\text{s}^2}$. We have

$$F = m * (ag + g)$$

where F is the engine thrust at lift-off, ag is the geometrical acceleration, and g is the acceleration of gravity on the planet. We find the launch mass is

$$m = \frac{F}{ag + g}$$

With $F = 61 \text{ kN}$, $ag = 20 \frac{\text{m}}{\text{s}^2}$ and $g = 9.8 \frac{\text{m}}{\text{s}^2}$ we get $2.0\text{e}3 \text{ kg}$.

10. The decomposition temperature graph is from Ventura and Wernimont²⁶³⁸ page 4.

40. Peter Madsen: "Ny hybrid motor, nu med Fessor II katalysator". In English,

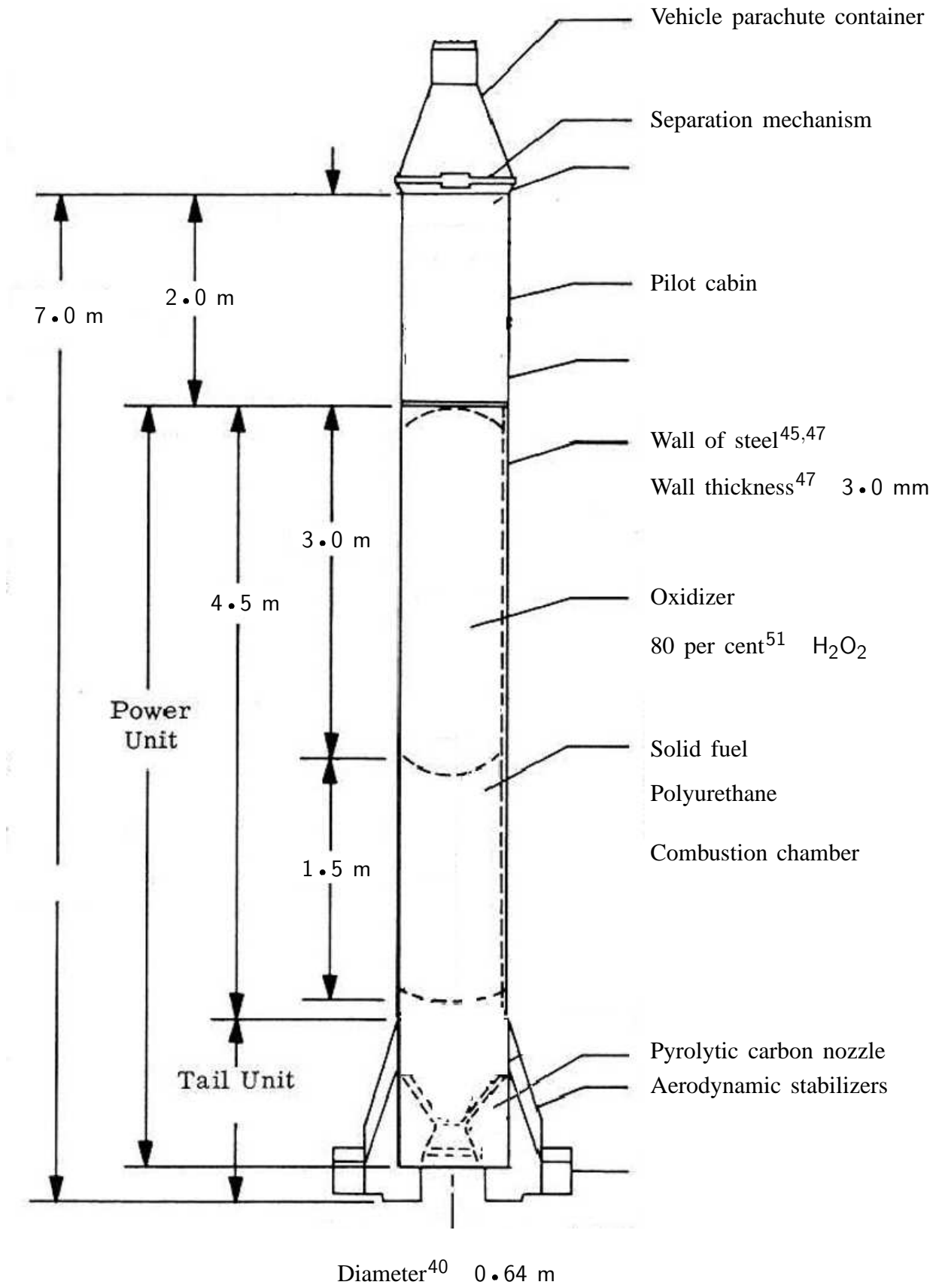
"New hybrid motor, now with Fessor II catalyst bed". Published by ing.dk 2014-09-02 13:43.

172. Mark, James E: "Polymer data handbook". Published by Oxford University Press, Inc, october 1998.

2638. Ventura, M C and Wernimont, Eric J: "Advancements in high concentration hydrogen peroxide catalyst beds". Published by AIAA as AIAA-01-3250, USA, July 2001.

2942. Datablad. Purteknik 1133 sort. Published by Edulan A/S, Denmark, June 2002.

2943. Sikkerhedsdatablad. Edulan Purteknik 1133 sort. Published by Edulan A/S, Denmark, 2003-03-24.



40. Peter Madsen: "Ny hybrid motor, nu med Fessor II katalysator". In English, "New hybrid motor, now with Fessor II catalyst bed". Published by ing.dk 2014-09-02 13:43.

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